

Numerical analysis of influence of ship hull form modification on ship resistance and propulsion characteristics

Part II Influence of hull form modification on wake current behind the ship

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ABSTRACT

After signing ship building contract shipyard's design office orders performance of ship resistance and propulsion model tests aimed at, apart from resistance measurements, also determination of ship speed, propeller rotational speed and propulsion engine power for the designed ship, as well as improvement of its hull form, if necessary. Range of ship hull modifications is practically very limited due to cost and time reasons. Hence numerical methods, mainly CFD ones are more and more often used for such tests. In this paper consisted of three parts, are presented results of numerical calculations of hull resistance, wake and efficiency of propeller operating in non-homogenous velocity field, performed for research on 18 hull versions of B573 ship designed and built by Szczecin Nowa Shipyard.

Keywords: ship hull geometry, numerical (computational) fluid dynamics, resistance, wake, propeller efficiency

NUMERICAL COMPUTATIONS OF WAKE CURRENT

The second effect of ship hull form modification, apart from change of resistance, is change of wake current which to a large extent influences performance of screw propeller (its thrust, torque and efficiency) as well as overall propulsive efficiency of ship.

Before commencing actual numerical computations a comparative test has been performed, namely, for the initial hull form of B 573 ship wake current has been numerically calculated and obtained results compared with its model tests.

Comparative test for wake current computations

Ship draught $T = 11.3$ [m]
Water density $\rho = 999.0$ [$\text{kg} \cdot \text{m}^{-3}$]
Kinematic viscosity $\nu = 1.13896$ [$\text{m}^2 \cdot \text{s}^{-1}$]

Wake fractions were determined in compliance with the axial component velocity V_x , according to the relation:

$$W_X = 1 - \frac{V_X}{V_M} \quad (2)$$

The computation results are presented graphically in Fig. 13 ÷ 16, and numerically - in Tab. 5. In Tab. 6 the results

of model tests [1] are given for comparison. The average value of wake fraction determined numerically within the range of values of the relative propeller radius r/R reaching from 0.25 to 1.21 is equal to 0.48, while that obtained from the model tests amounts to 0.52.

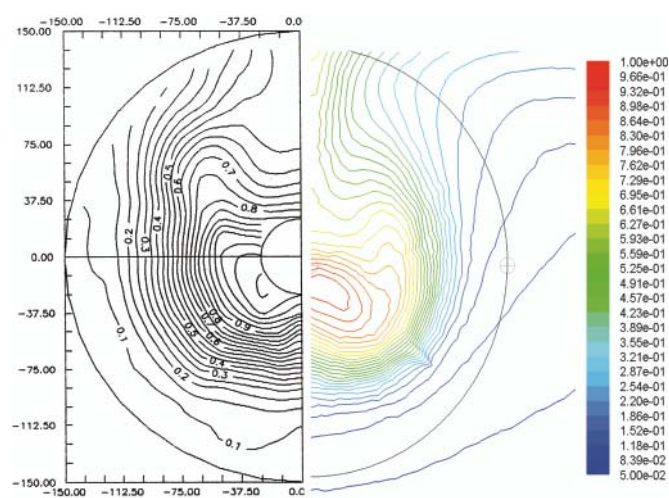


Fig. 13. Axial wake fraction distribution on the propeller disk plane: on the right side – results of the numerical test, on the left side – results of the model test [1]

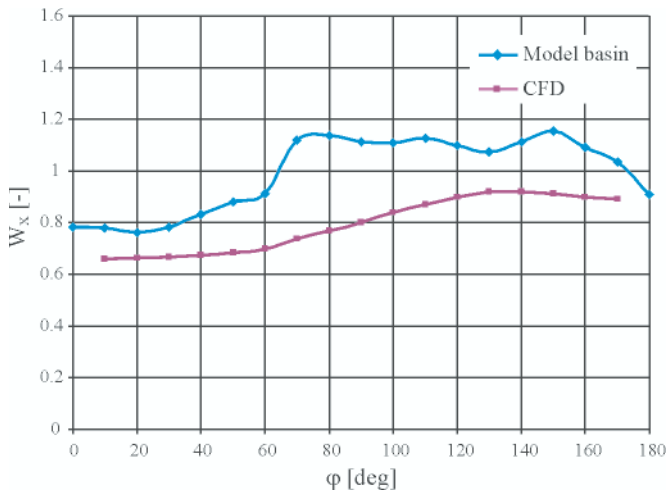


Fig. 14. Circumferential distribution of axial wake fraction component for $r/R = 0.202$

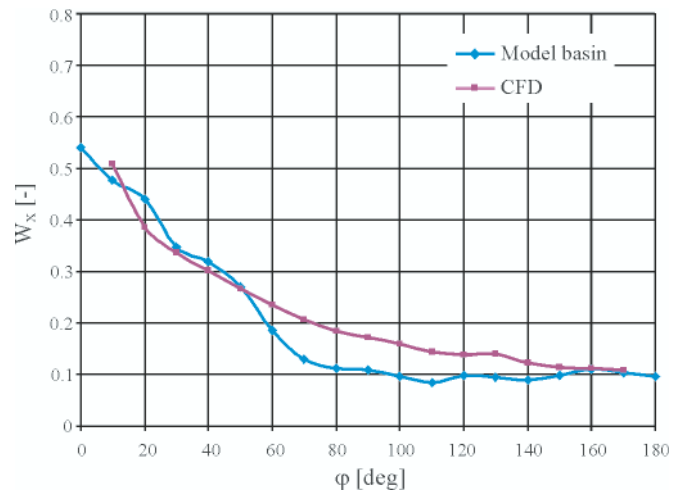


Fig. 16. Circumferential distribution of axial wake fraction component for $r/R = 1.0$

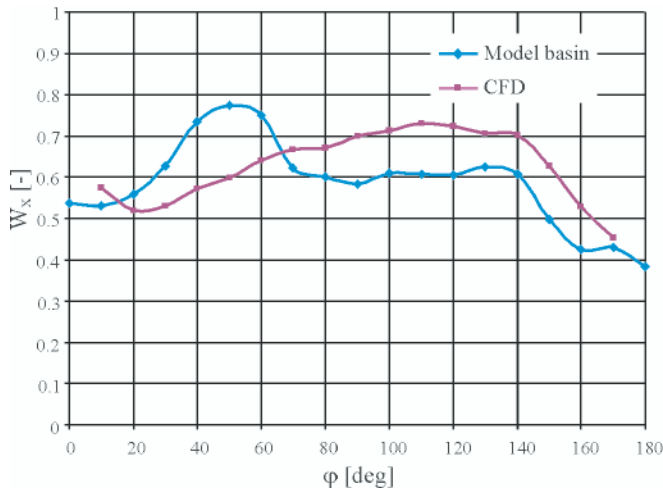


Fig. 15. Circumferential distribution of axial wake fraction component for $r/R = 0.60$

In Fig. 17 stream lines for the initial ship hull form are also shown.

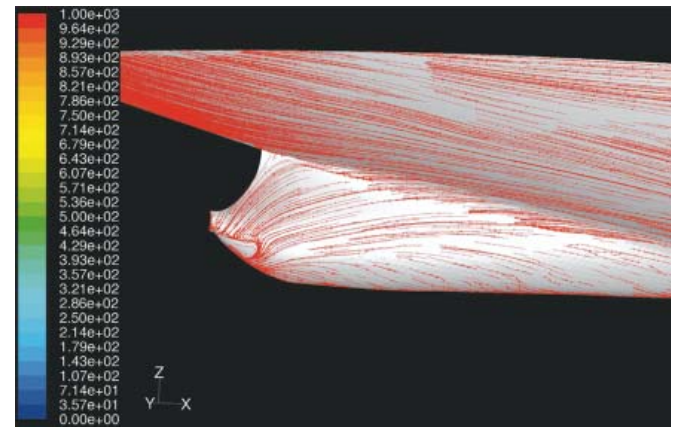


Fig. 17. Distribution of stream lines on ship hull model

Tab. 5. Results of numerical calculations of the axial wake fraction component $W_x [-]$

| r [mm] | 25 | 37.5 | 50 | 62.5 | 75 | 87.5 | 100 | 112.5 | 125 | 137.5 | 150 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| phi [deg] | | | | | | | | | | | |
| 10 | 0.6595 | 0.6383 | 0.6212 | 0.5977 | 0.5746 | 0.5451 | 0.521 | 0.5108 | 0.5094 | 0.5092 | 0.5389 |
| 20 | 0.6627 | 0.6353 | 0.5994 | 0.5658 | 0.52 | 0.4793 | 0.4383 | 0.4079 | 0.3853 | 0.3747 | 0.3787 |
| 30 | 0.6663 | 0.6316 | 0.6004 | 0.5676 | 0.5306 | 0.4839 | 0.4268 | 0.3783 | 0.337 | 0.3139 | 0.3028 |
| 40 | 0.6738 | 0.6365 | 0.615 | 0.5968 | 0.572 | 0.507 | 0.427 | 0.3485 | 0.3015 | 0.2709 | 0.2562 |
| 50 | 0.6843 | 0.6476 | 0.6449 | 0.6427 | 0.5997 | 0.5153 | 0.4162 | 0.3163 | 0.266 | 0.2385 | 0.2195 |
| 60 | 0.6998 | 0.674 | 0.6692 | 0.6786 | 0.6395 | 0.5285 | 0.3882 | 0.2989 | 0.2355 | 0.2072 | 0.1906 |
| 70 | 0.7364 | 0.6949 | 0.702 | 0.7093 | 0.6676 | 0.5308 | 0.3962 | 0.262 | 0.2073 | 0.1817 | 0.1677 |
| 80 | 0.7674 | 0.7267 | 0.7221 | 0.7351 | 0.6703 | 0.5154 | 0.3919 | 0.2507 | 0.1838 | 0.1636 | 0.1488 |
| 90 | 0.8005 | 0.7552 | 0.7469 | 0.7587 | 0.7001 | 0.5467 | 0.3797 | 0.2505 | 0.1715 | 0.1467 | 0.1347 |
| 100 | 0.8391 | 0.804 | 0.7794 | 0.781 | 0.7121 | 0.566 | 0.3707 | 0.2258 | 0.1601 | 0.1344 | 0.1225 |
| 110 | 0.871 | 0.8441 | 0.8131 | 0.7976 | 0.7299 | 0.5715 | 0.3586 | 0.2128 | 0.1436 | 0.1236 | 0.113 |
| 120 | 0.8992 | 0.8773 | 0.8404 | 0.8161 | 0.7236 | 0.5745 | 0.3484 | 0.1958 | 0.1391 | 0.1158 | 0.1053 |
| 130 | 0.9197 | 0.9042 | 0.8653 | 0.8176 | 0.7064 | 0.5448 | 0.3567 | 0.2119 | 0.1397 | 0.1101 | 0.0992 |
| 140 | 0.9204 | 0.9083 | 0.8645 | 0.8055 | 0.7012 | 0.4911 | 0.2737 | 0.1681 | 0.1227 | 0.1033 | 0.0943 |
| 150 | 0.9114 | 0.8791 | 0.8406 | 0.7467 | 0.6279 | 0.4252 | 0.254 | 0.1511 | 0.1143 | 0.1001 | 0.0909 |
| 160 | 0.8998 | 0.8588 | 0.8035 | 0.7018 | 0.5283 | 0.3518 | 0.2067 | 0.1414 | 0.1122 | 0.0989 | 0.0897 |
| 170 | 0.8927 | 0.8361 | 0.7455 | 0.6106 | 0.4542 | 0.2885 | 0.18 | 0.129 | 0.1088 | 0.0969 | 0.088 |

Tab.6. Results of model tests of the axial wake fraction component W_x [-]

| r/R | 0.202 | 0.25 | 0.3 | 0.35 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 0.95 | 1 | 1.21 |
|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| r [mm] | 25 | 31 | 37.2 | 43.4 | 49.6 | 62 | 74.4 | 86.8 | 99.2 | 111.6 | 117.8 | 124 | 150 |
| φ [deg] | | | | | | | | | | | | | |
| 0 | 0.783 | 0.736 | 0.692 | 0.652 | 0.617 | 0.566 | 0.537 | 0.531 | 0.535 | 0.537 | 0.538 | 0.540 | 0.570 |
| 10 | 0.778 | 0.731 | 0.686 | 0.646 | 0.612 | 0.562 | 0.531 | 0.516 | 0.506 | 0.492 | 0.484 | 0.478 | 0.466 |
| 20 | 0.763 | 0.715 | 0.671 | 0.633 | 0.604 | 0.570 | 0.559 | 0.551 | 0.526 | 0.485 | 0.463 | 0.440 | 0.359 |
| 30 | 0.784 | 0.741 | 0.702 | 0.670 | 0.646 | 0.626 | 0.628 | 0.611 | 0.537 | 0.433 | 0.387 | 0.348 | 0.250 |
| 40 | 0.830 | 0.797 | 0.767 | 0.744 | 0.727 | 0.718 | 0.734 | 0.702 | 0.583 | 0.432 | 0.369 | 0.319 | 0.197 |
| 50 | 0.881 | 0.857 | 0.835 | 0.816 | 0.801 | 0.785 | 0.774 | 0.701 | 0.552 | 0.389 | 0.323 | 0.270 | 0.152 |
| 60 | 0.913 | 0.893 | 0.874 | 0.856 | 0.840 | 0.807 | 0.750 | 0.630 | 0.458 | 0.294 | 0.232 | 0.186 | 0.116 |
| 70 | 1.119 | 1.121 | 1.105 | 1.068 | 1.005 | 0.814 | 0.623 | 0.458 | 0.312 | 0.198 | 0.157 | 0.130 | 0.111 |
| 80 | 1.138 | 1.141 | 1.122 | 1.079 | 1.006 | 0.789 | 0.600 | 0.438 | 0.291 | 0.177 | 0.138 | 0.112 | 0.104 |
| 90 | 1.111 | 1.113 | 1.098 | 1.063 | 1.005 | 0.817 | 0.584 | 0.391 | 0.253 | 0.157 | 0.126 | 0.108 | 0.111 |
| 100 | 1.108 | 1.109 | 1.095 | 1.061 | 1.005 | 0.824 | 0.610 | 0.423 | 0.271 | 0.157 | 0.119 | 0.097 | 0.112 |
| 110 | 1.127 | 1.130 | 1.113 | 1.073 | 1.005 | 0.802 | 0.608 | 0.438 | 0.281 | 0.155 | 0.112 | 0.084 | 0.087 |
| 120 | 1.099 | 1.101 | 1.088 | 1.057 | 1.004 | 0.832 | 0.605 | 0.408 | 0.263 | 0.157 | 0.121 | 0.098 | 0.089 |
| 130 | 1.073 | 1.074 | 1.065 | 1.042 | 1.003 | 0.865 | 0.626 | 0.415 | 0.266 | 0.153 | 0.116 | 0.094 | 0.104 |
| 140 | 1.112 | 1.114 | 1.099 | 1.064 | 1.005 | 0.819 | 0.607 | 0.422 | 0.271 | 0.155 | 0.115 | 0.089 | 0.083 |
| 150 | 1.156 | 1.159 | 1.138 | 1.089 | 1.007 | 0.754 | 0.498 | 0.302 | 0.182 | 0.124 | 0.109 | 0.099 | 0.088 |
| 160 | 1.090 | 1.080 | 1.049 | 0.991 | 0.902 | 0.650 | 0.426 | 0.263 | 0.167 | 0.128 | 0.118 | 0.110 | 0.091 |
| 170 | 1.034 | 1.018 | 0.985 | 0.932 | 0.856 | 0.643 | 0.429 | 0.261 | 0.161 | 0.121 | 0.111 | 0.103 | 0.079 |
| 180 | 0.909 | 0.876 | 0.834 | 0.783 | 0.721 | 0.565 | 0.383 | 0.226 | 0.134 | 0.103 | 0.098 | 0.096 | 0.079 |

RESULTS OF ANALYSIS OF WAKE CURRENT FOR MODIFIED VERSIONS OF SHIP HULL

Numerical calculations of wake current were performed for the same modified ship hull versions as in the case of the resistance investigations (Tab. 2).

The ship hull model speed $V = 1.492$ [m/s].

The collected results of numerical calculations in the form of the average wake fraction according to Eq. (2), are given in Tab. 7.

The influence of particular modified geometrical parameters of ship hull model on the average value of wake fraction is presented in Figs. 18 ÷ 20, and, in Fig. 21 and 22 are given circumferential distributions of axial and tangential wake fraction components for $r/R = 0,6$.

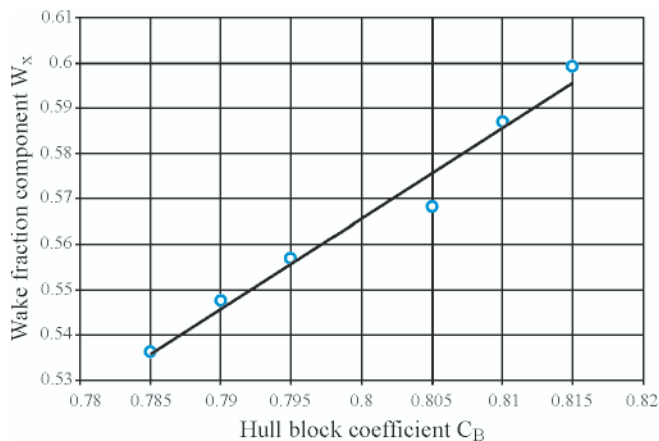


Fig. 18. Wake fraction component W_x calculated in function of C_B

Tab. 7. Average values of axial wake fraction for modified hull versions of B 573 ship

| Number of variant | Modified parameter | Average value of axial wake fraction |
|-------------------|---------------------|--------------------------------------|
| | C_B | W_x |
| 1 | 0.79 | 0.547 |
| 2 | 0.795 | 0.556 |
| 3 | 0.785 | 0.536 |
| 4 | 0.81 | 0.586 |
| 5 | 0.805 | 0.568 |
| 6 | 0.815 | 0.599 |
| | C_p | |
| 7 | 0.78 | 0.539 |
| 8 | 0.77 | 0.523 |
| 9 | 0.76 | 0.507 |
| 10 | 0.8 | 0.578 |
| 11 | 0.81 | 0.602 |
| | LCB | |
| 12 | 47% | 0.517 |
| 13 | 46% | 0.491 |
| 14 | 45% | 0.468 |
| 15 | 49% | 0.593 |
| 16 | 50% | 0.620 |
| 17 | 51% | 0.681 |
| 18 | Manual modification | 0.471 |

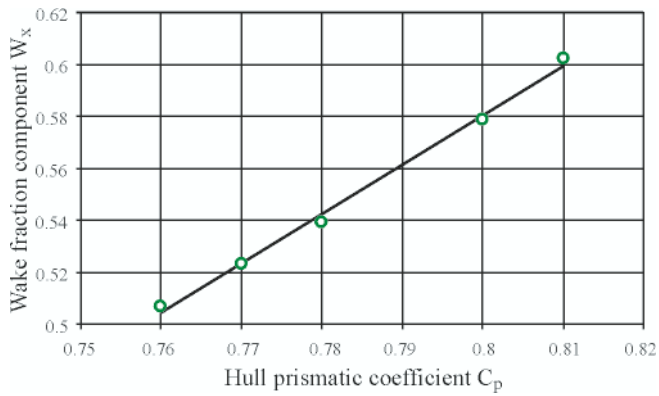


Fig. 19. Wake fraction component W_x calculated in function of C_p

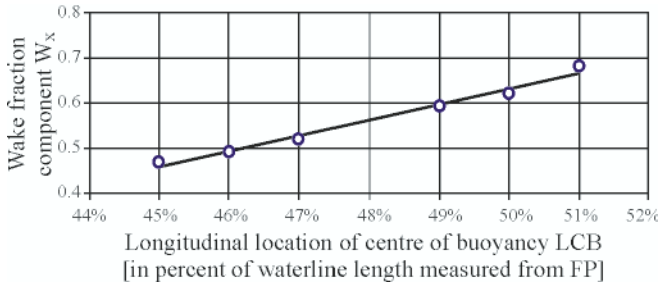


Fig. 20. Wake fraction component W_x calculated in function of LCB

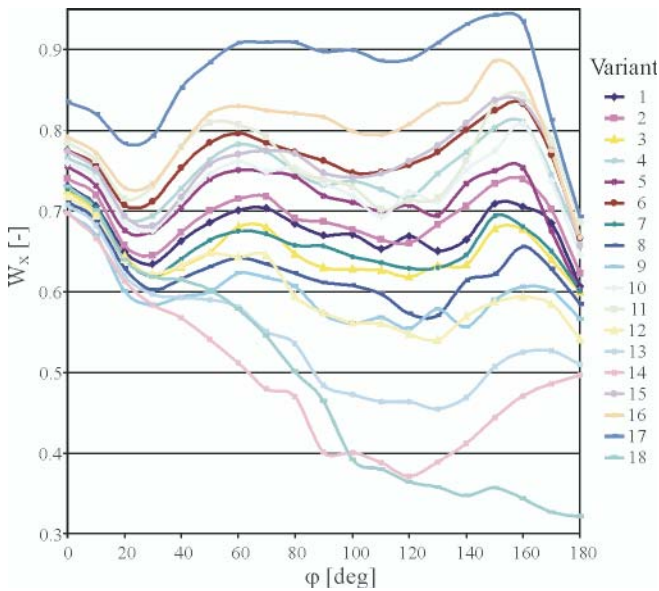


Fig. 21. Circumferential distribution of field of the axial wake fraction component for $r/R = 0.6$, calculated for all the analyzed variants (18 in number)

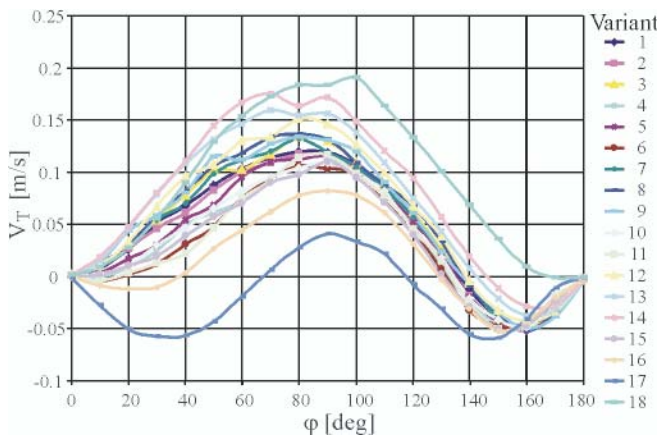
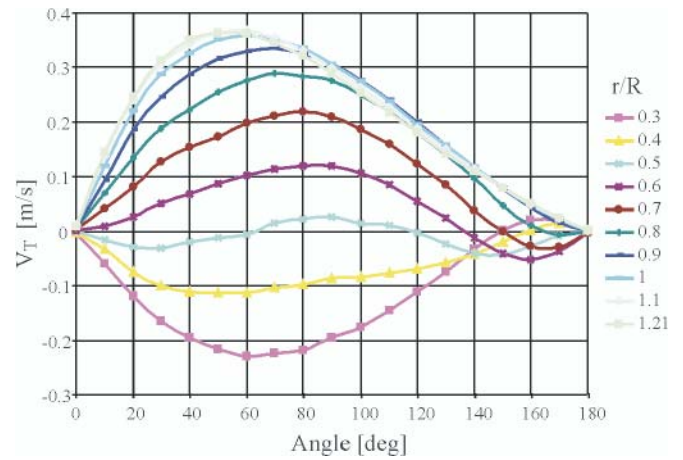
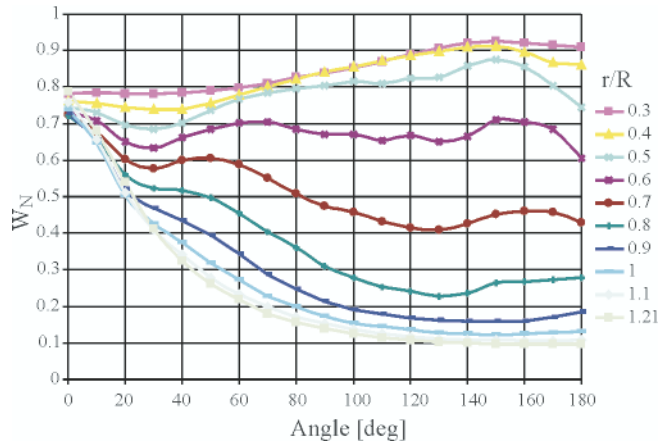


Fig. 22. Circumferential distribution of field of the tangential velocity component for $r/R = 0.6$, calculated for all the analyzed variants (18 in number)

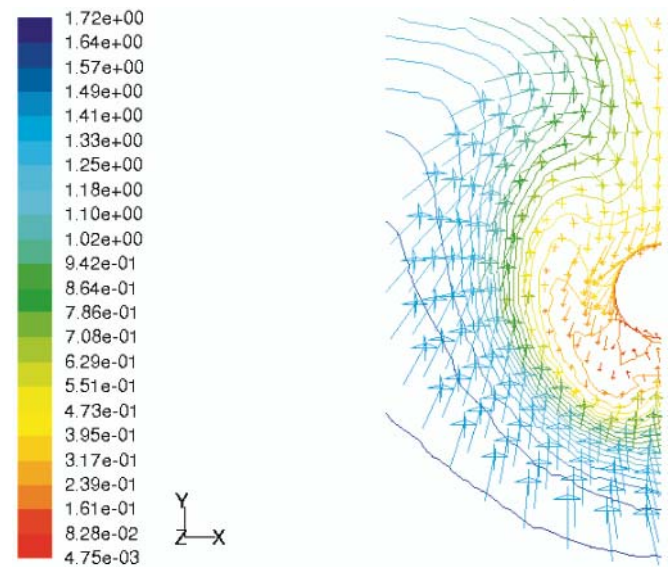
In Figs. 23 ÷ 29 are exemplified distributions of tangential and axial wake fractions as well as velocity vectors on the propeller disk plane for selected variants of B 573 ship hull modification. The complete set of numerical calculation results is contained in the report on the research project [2].



Distribution of the tangential velocity V_T

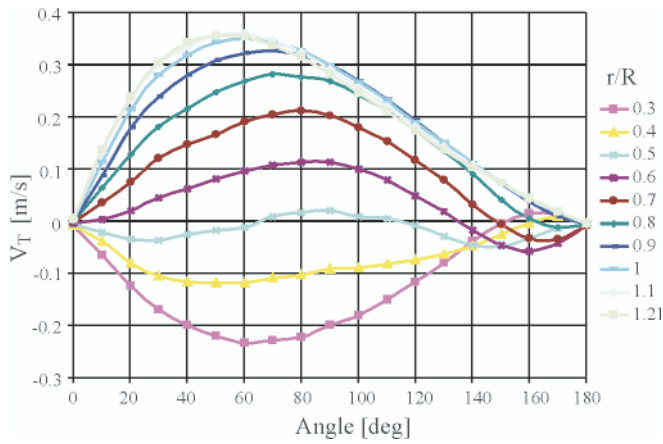


Distribution of the axial wake fraction component W_N

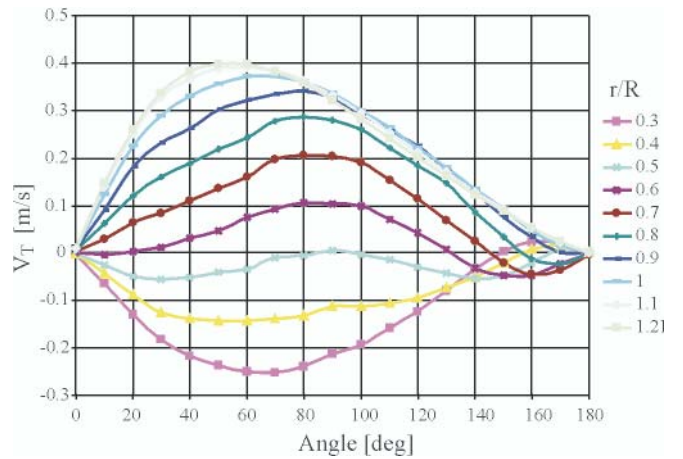


Wake current velocity vectors

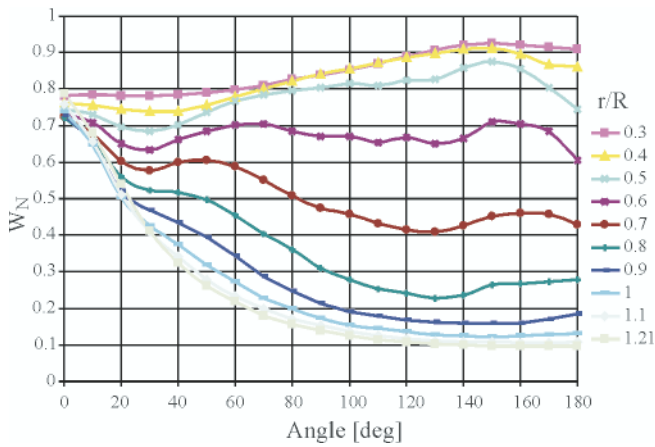
Fig. 23. Distributions of tangential velocities and axial wake fraction as well as velocity vectors in propeller disk plane for variant 1 of B 573 ship hull modification



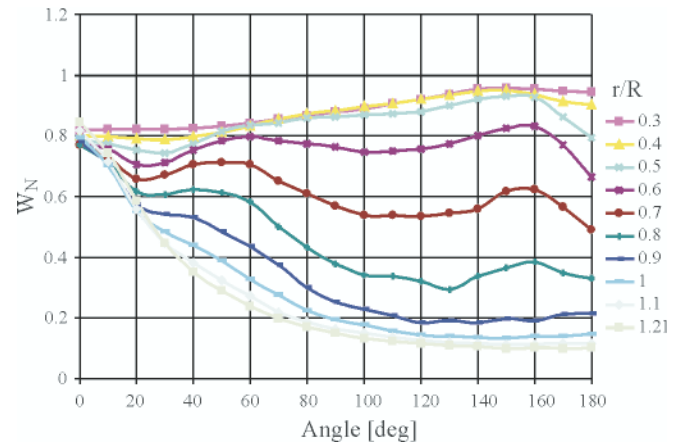
Distribution of the tangential velocity V_T



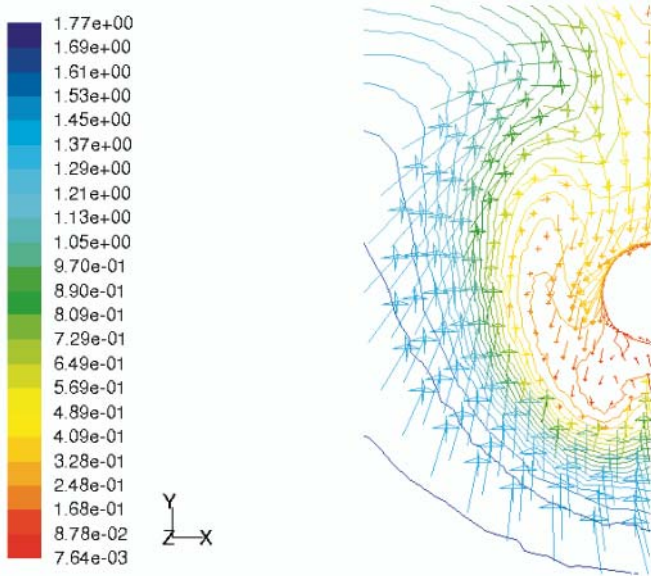
Distribution of the tangential velocity V_T



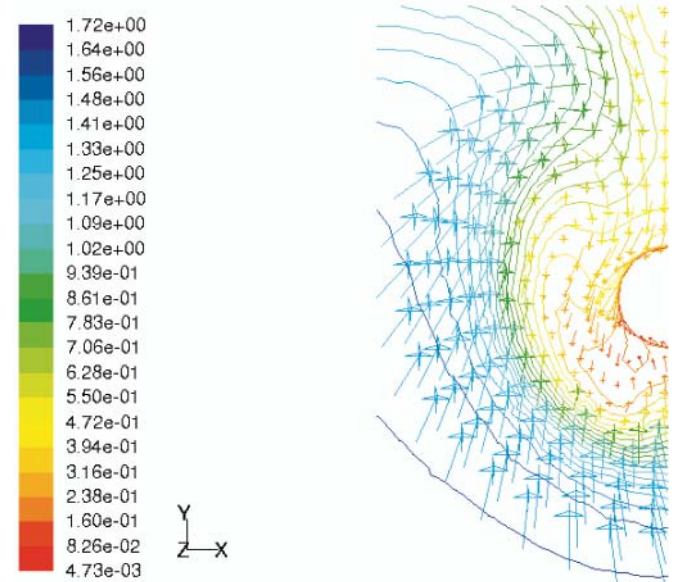
Distribution of the axial wake fraction component W_N



Distribution of the axial wake fraction component W_N



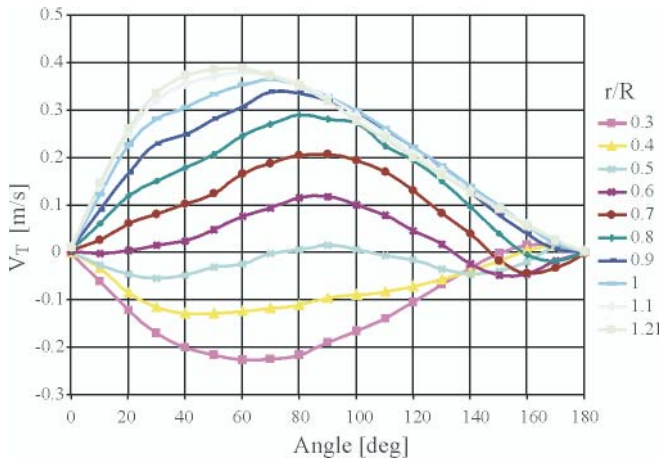
Wake current velocity vectors



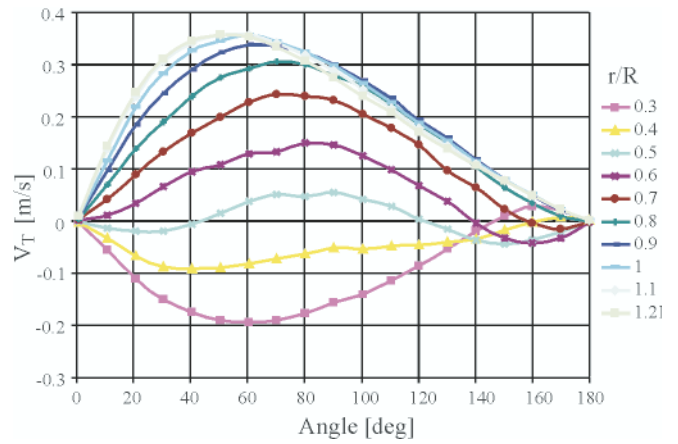
Wake current velocity vectors

Fig. 24. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 6 of B 573 ship hull modification

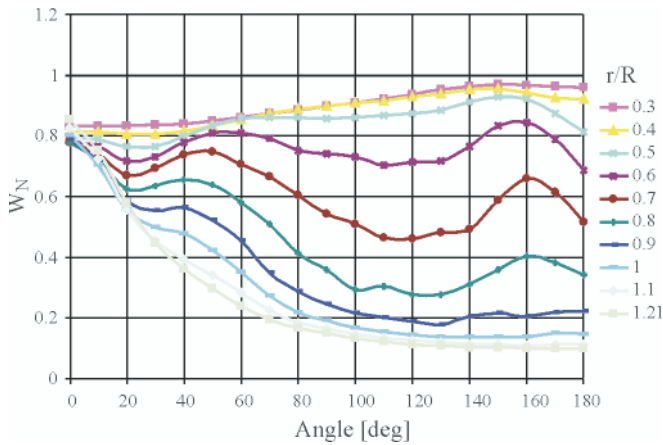
Fig. 25. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 7 of B 573 ship hull modification



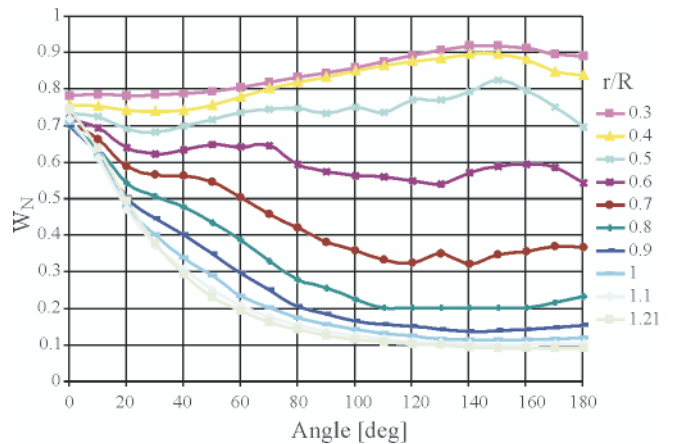
Distribution of the tangential velocity V_T



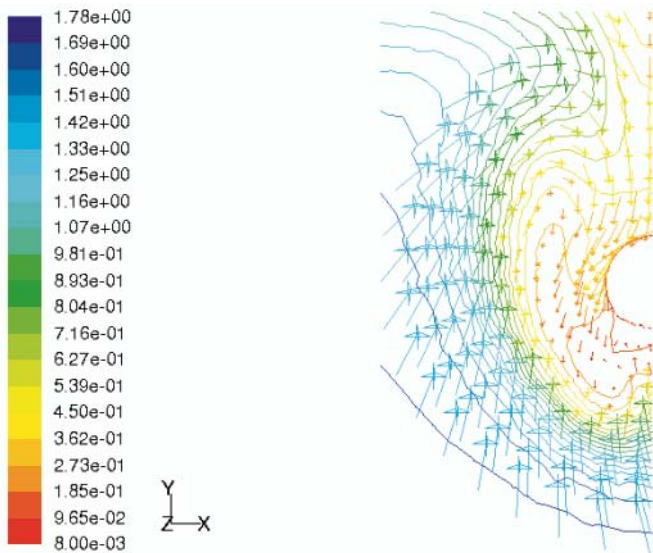
Distribution of the tangential velocity V_T



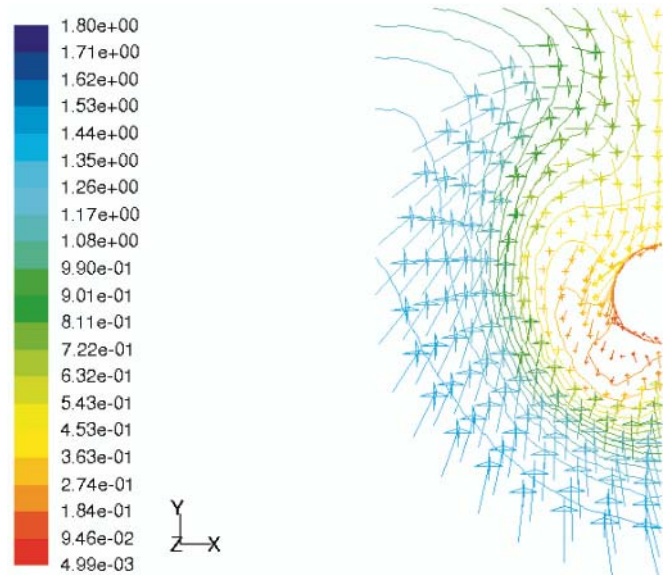
Distribution of the axial wake fraction component W_N



Distribution of the axial wake fraction component W_N



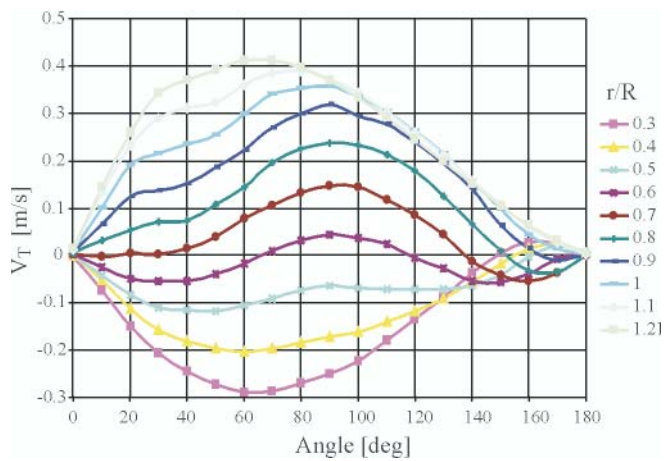
Wake current velocity vectors



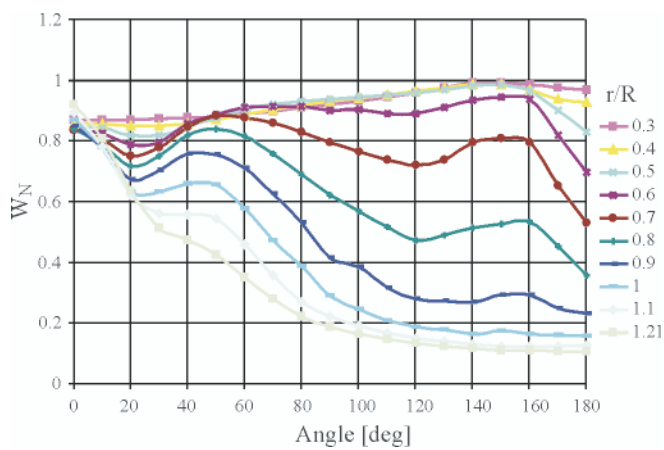
Wake current velocity vectors

Fig. 26. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 11 of B 573 ship hull modification

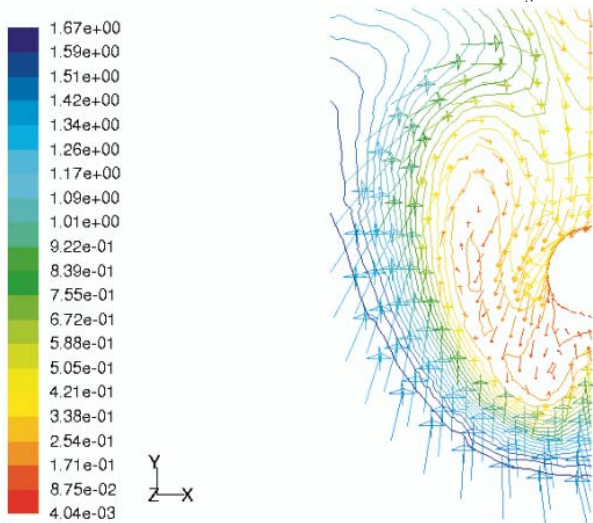
Fig. 27. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 12 of B 573 ship hull modification



Distribution of the tangential velocity V_T

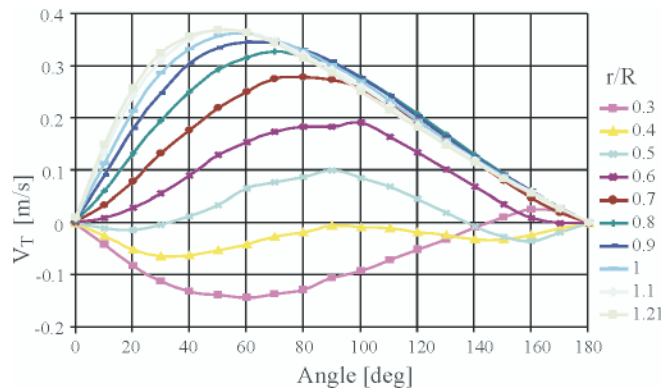


Distribution of the axial wake fraction component W_N

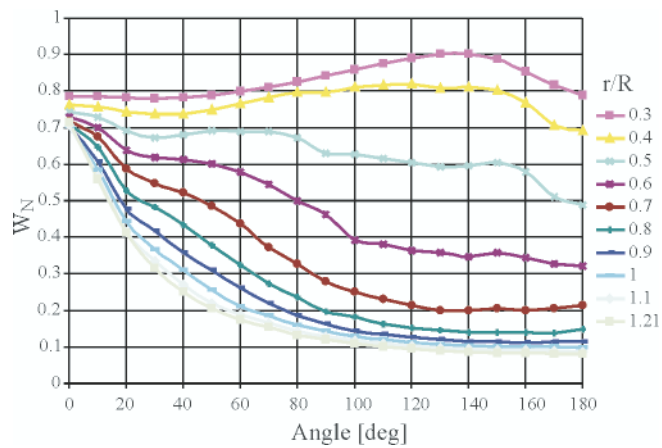


Wake current velocity vectors

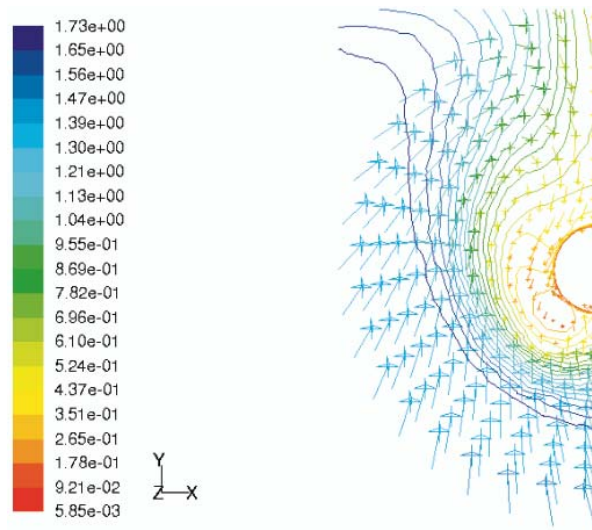
Fig. 28. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 17 of B 573 ship hull modification



Distribution of the tangential velocity V_T



Distribution of the axial wake fraction component W_N



Wake current velocity vectors

Fig. 29. Distributions of tangential velocities and axial wake fraction as well as velocity vectors on propeller disk plane for variant 18 of B 573 ship hull modification

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- Szelangiewicz T.: *Numerical investigations on ship rudder-propeller-stern co-operation aimed at the improving of*

transport ship propulsion and manoeuvrability properties (in Polish). Appendix to the final report on realization of the development project No. R 10 008 01, Szczecin 2009.

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